



First-principles studies of Ni–Ta intermetallic compounds

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ABSTRACT

The structural properties, heats of formation, elastic properties, and electronic structures of Ni–Ta intermetallic compounds are investigated in detail based on density functional theory. Our results indicate that all Ni–Ta intermetallic compounds calculated here are mechanically stable except for P21/m-Ni₃Ta and hc-NiTa₂. Furthermore, we found that Pmmn-Ni₃Ta is the ground state stable phase of Ni₃Ta polymorphs. The polycrystalline elastic modulus has been deduced by using the Voigt–Reuss–Hill approximation. All Ni–Ta intermetallic compounds in our study, except for NiTa, are ductile materials by corresponding *G/K* values and poisson's ratio. The calculated heats of formation demonstrated that Ni₂Ta are thermodynamically unstable. Our results also indicated that all Ni–Ta intermetallic compounds analyzed here are conductors. The density of state demonstrated the structure stability increases with the Ta concentration.

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1. Introduction

Due to the high melting temperature, excellent properties in harsh environments, Ni–Ta alloys stand out as remarkable candidates for high-temperature materials [1], and they are highly attractive from scientific and technological points of view [2]. The first Ni–Ta phase diagram was published by Therkelsen [3] in 1933. After that, a substantial number of papers on Ni–Ta intermetallic phases has been published. Notably, in 1984, Nash et al. [4], pointed out that five intermetallic phases and two terminal solid solutions, FCC (Ni) and BCC (Ta) existing in Ni–Ta phases diagram. In 1991 and 1994, thermodynamic properties of this system were evaluated by adopting the CALPHAD approach by Kaufman [5] and Ansara et al. [6], respectively. In 1999, the Ni–Ta binary system was reassessed by Cui et al. [7] and a set of parameters describing the Gibbs energy of each phase was obtained through the CALPHAD method. In 2002, the phase equilibrium relationship and thermodynamic properties were analyzed by Pan et al. [1] by adopting the diffusion and EPMA methods. In 2009, the Gibbs free energy functions were evaluated and the associated equilibrium phase diagram was reported by Zhou et al. [8] by combining the CALPHAD method and first-principle calculations. Based on Ni–Ta phase diagrams studied by these researchers, it was revealed that five kinds of intermetallic

compounds exist in the Ni–Ta system, namely, Ni₈Ta, Ni₃Ta, Ni₂Ta, NiTa, and NiTa₂.

Despite these efforts [8–10], there are a number of remaining long-standing questions about crystal structures and properties of Ni–Ta intermetallic compounds. For instance, it is known that Ni₃Ta has three polymorphs (Pmmn-Ni₃Ta with space group of Pmmn, I4/mmm-Ni₃Ta with space group of I4/mmm and P21/m-Ni₃Ta with space group of P21/m [4,8,11–16]) at different temperatures conditions. However, which polymorph is the ground stable phase is still a controversy. In addition, the mechanism of shape memory effect of Ni₃Ta is still unclear. In order to uncover this mechanism, a study of intrinsic ductility and brittleness of Ni₃Ta is needed. Furthermore, the crystal structures of Ni₈Ta [4] and NiTa₂ [17,18] are undetermined to date, and a further study in this direction is required. Comprehensive studied on other properties of these alloys are lacking in the literatures, and composite dependent mechanical properties of Ni–Ta intermetallic compounds are missing. To fill in these gaps, in this work we undertake a systematical analysis of the structural, thermodynamic, mechanical, and electronic properties of the Ni–Ta intermetallic compounds by adopting first-principles calculations.

2. Computational method

In this work, five kinds of Ni–Ta intermetallic compounds and the corresponding eight crystal structures (namely, Ni₈Ta, I4/mmm-Ni₃Ta, Pmmn-Ni₃Ta, P21/m-Ni₃Ta, Ni₂Ta, NiTa, ha-NiTa₂ with ha Wyckoff atomic positions, and hc-NiTa₂ with hc Wyckoff

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atomic positions) have been considered. First-principles calculations have been performed by employing the CASTEP package [19], in which density functional theory (DFT) and the plane-wave pseudopotential technique are implemented. The ion–electron interaction is modeled by the ultrasoft pseudopotential method [20]. The generalized gradient approximation (GGA) [21] with the Perdew–Burke–Ernzerhof (PBE) [22] exchange–correlation functional has been used in the process of calculation. The kinetic cutoff energy for plane waves has been set as 400 eV [23]. The \mathbf{k} point separation in the Brillouin zone of the reciprocal space is 0.07 nm^{-1} , that is, $4 \times 4 \times 5$ for $I4/mmm\text{-Ni}_3\text{Ta}$, $3 \times 3 \times 3$ for NiTa, $5 \times 5 \times 6$ for Ni_2Ta , $4 \times 4 \times 3$ for $ha\text{-NiTa}_2$, $4 \times 4 \times 3$ for $hc\text{-NiTa}_2$, $4 \times 4 \times 3$ for Ni_8Ta , and $3 \times 3 \times 3$ for $\text{Pmmn-Ni}_3\text{Ta}$, $3 \times 3 \times 2$ for $\text{P21/m-Ni}_3\text{Ta}$, respectively. A relationship between Ni_2Ta primitive cell total energy and plane-wave cutoff energy was calculated to determine an appropriate cutoff energy for the plane-wave basis set. It is displayed obviously in Fig. 1 that the total energy

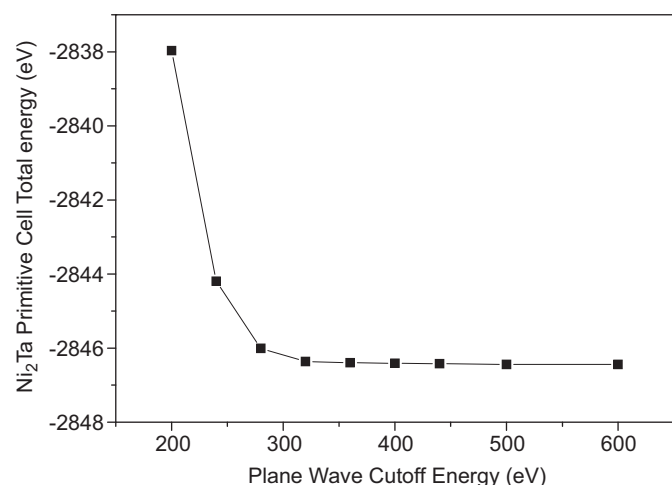


Fig. 1. The relationship between Ni_2Ta primitive cell total energy and plane-wave cutoff energy.

changes little with the increasing of cutoff energy which exceeds 360 eV. Therefore, a cutoff energy of 400 eV is selected in this work.

Benchmark calculations have been performed for the Ni_2Ta phase, pointing out that the computational scheme utilized in this work is credible. Indeed, the calculated lattice parameter of $a=0.3196 \text{ nm}$, $c=0.8174 \text{ nm}$ compares well with the experimental value of $a=0.3160 \text{ nm}$ and $c=0.7950 \text{ nm}$ [24], $a=0.3154 \text{ nm}$ and $c=0.7905 \text{ nm}$ [25].

3. Results and discussion

3.1. Structural properties

By applying the experimental crystallographic data of the Ni–Ta intermetallic compounds from Refs. [4,8,11–18,24–35] as the original configurations, the lattice parameters and internal coordinates of the Ni–Ta intermetallic compounds have been optimized. The Convergence tolerance of energy, force, stress and displacement for Ni–Ta alloys are $1 \times 10^{-5} \text{ eV/atom}$, 0.03 eV/atom , 0.05 GPa and 0.001 \AA , respectively. The calculated lattice parameters and the corresponding mass densities, together with the experimental [17–18,24–25,29–32,34–35] data, are shown in Table 1. As shown in Table 1, the lattice parameters and mass densities of all Ni–Ta intermetallic compounds agree perfectly with the corresponding experimental ones. This observation is an additional confirmation that the computational methodology adopted in this paper is suitable for the purpose of this study and the accuracy of our geometry optimizations is sufficient.

In Fig. 2, the calculated mass densities of Ni–Ta intermetallic compounds are plotted with corresponding existing experimental values. We observe that the mass density of Ni–Ta intermetallic compounds keeps a linear growth with Ta concentration c (in at %). The relationship between the mass density (in g/cm^3) and the Ta concentration c (in at %) can be described by the following formula: $\rho=9.38889+6.82437 c$. As it is shown in Figure 1, the calculated values of densities correspond satisfyingly with the experimental ones, which verifies the reliability of the calculation results.

Table 1

Theoretical lattice parameters and mass density compared to experimental values for the Ni–Ta intermetallic compounds.

Compound	Space group	Mass density (g/cm^3)	Lattice parameters (nm)	Reference
Ni	Fm-3m	8.842	$a=0.3531$	This work
		8.970	$a=0.3515$	[36]
		8.910	$a=0.3524$	[37]
Ni_8Ta	$I4/mmm$	10.061	$a=0.7692, c=0.3623$	This work
		11.422	$a=0.3724, c=0.7527$	This work
		12.090	$a=0.3627, c=0.7455$	[31]
$\text{Pmmn-Ni}_3\text{Ta}$	Pmmn	11.444	$a=0.5181, b=0.4327, c=0.4622$	This work
		12.130	$a=0.5122, b=0.4522, c=0.4235$	[32]
		11.383	$a=0.4612, b=0.5209, c=0.8804$	This work
$\text{P21/m-Ni}_3\text{Ta}$	P21/m	12.040	$a=0.4532, b=0.5125, c=0.8632$	[30]
		11.870	$a=0.3196, c=0.8174$	This work
		12.480	$a=0.3160, c=0.7950$	[24]
Ni_2Ta	$I4/mmm$	12.600	$a=0.3154, c=0.7905$	[25]
		13.168	$a=0.4936, c=2.6834$	This work
		13.750	$a=0.4921, c=2.6905$	[29]
$ha\text{-NiTa}_2$	$I4/mcm$	14.157	$a=0.6355, c=0.4887$	This work
		14.960	$a=0.6197, c=0.4869$	[17]
		13.532	$a=0.6742, c=0.4542$	This work
$hc\text{-NiTa}_2$	$I4/mcm$	14.840	$a=0.6216, c=0.4872$	[18]
		15.773	$a=0.3365$	This work
		16.630	$a=0.3306$	[39]
Ta	Im-3m	16.670	$a=0.3303$	[40]
				[41]

3.2. Elastic properties and mechanical stability

In this work, the elastic constants C_{ij} (GPa) and bulk modulus of the Ni–Ta intermetallic compounds have been evaluated, and the calculation results are summarized in Table 2. The mechanical stability of the Ni–Ta intermetallic compounds are studied through a mechanical stability criterion, known from the literature.

In particular, for monoclinic crystal, the conditions for mechanical stability are given by [42]:

$$C_{ij} > 0 (i=j, 0 < i \leq 6), C_{33}C_{55} - C_{35}^2 > 0, C_{44}C_{66} - C_{46}^2 > 0, C_{22}C_{33} - C_{23}^2 > 0, \\ C_{11} + C_{22}C_{33} + 2(C_{12} + C_{13} + C_{23}) > 0, \\ [C_{22}(C_{33}C_{55} - C_{35}^2) + 2(C_{23}C_{25}C_{35} - C_{25}^2C_{55} - C_{25}^2C_{33})] > 0, \\ \{2[C_{15}C_{25}(C_{33}C_{12} - C_{13}C_{23}) + C_{15}C_{35}(C_{22}C_{13} - C_{12}C_{23}) \\ + C_{25}C_{35}(C_{11}C_{23} - C_{12}C_{23})] - [C_{25}^2(C_{22}C_{33} - C_{23}^2) + C_{25}^2(C_{11}C_{33} - C_{23}^2)]\} > 0.$$

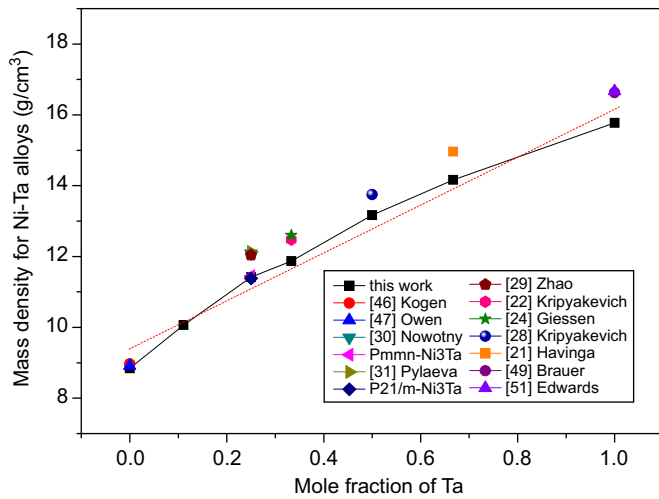


Fig. 2. Theoretical mass density compared to experimental values for the Ni–Ta intermetallic compounds.

Table 2

Calculated elastic properties for the single crystalline Ni–Ta intermetallic compounds.

Compound	Elastic properties
Ni ₈ Ta	$C_{11}=305, C_{12}=139, C_{13}=186, C_{16}=0, C_{33}=259, C_{44}=117, C_{66}=54, K=210$
I4/mmm-Ni ₃ Ta	$C_{11}=281, C_{12}=202, C_{13}=167, C_{16}=0, C_{33}=353, C_{44}=112, C_{66}=157, K=220$
Pmmn-Ni ₃ Ta	$C_{11}=388, C_{12}=109, C_{13}=144, C_{23}=148, C_{22}=376, C_{33}=367, C_{44}=81, C_{55}=102, C_{66}=70, K=215$
P21/m-Ni ₃ Ta	$C_{11}=364, C_{12}=141, C_{13}=148, C_{15}=7, C_{23}=125, C_{25}=-14, C_{35}=14, C_{46}=-18, C_{22}=384, C_{33}=350, C_{44}=69, C_{55}=80, C_{66}=83, K=214$
Ni ₂ Ta	$C_{11}=253, C_{12}=214, C_{13}=158, C_{16}=0, C_{33}=356, C_{44}=86, C_{66}=144, K=212$
NiTa	$C_{11}=363, C_{12}=151, C_{13}=130, C_{33}=388, C_{44}=113, K=215$
ha-NiTa ₂	$C_{11}=395, C_{12}=173, C_{13}=131, C_{16}=0, C_{33}=394, C_{44}=16, C_{66}=74, K=204$
hc-NiTa ₂	$C_{11}=-565, C_{12}=979, C_{13}=226, C_{16}=0, C_{33}=315, C_{44}=-77, C_{66}=74, K=202$

C_{ij} , elastic constants (in GPa); K , bulk modulus (in GPa).

Table 3

Polycrystalline bulk modulus, shear modulus, Young's modulus (GPa), Poisson's ratios and valence electron densities (electron/Å³) for mechanically stable Ni–Ta intermetallic compounds according to Voigt–Reuss–Hill approximation. K is the bulk modulus (in GPa); G is the shear modulus (in GPa); E is Young's modulus (in GPa); ν is Poisson's ratio.

Compound	K_V	K_R	K_H	G_V	G_R	G_H	E	G/K	ν	Valence electron density
Ni ₈ Ta	210	210	210	81	66	74	199	0.35	0.3424	0.193
I4/mmm-Ni ₃ Ta	221	220	220	101	82	92	242	0.42	0.3174	0.224
Pmmn-Ni ₃ Ta	215	215	215	99	94	96	252	0.45	0.3042	0.212
Ni ₂ Ta	213	212	213	85	54	70	189	0.33	0.3526	0.227
NiTa	215	215	215	113	112	113	288	0.53	0.2765	0.242
ha-NiTa ₂	206	205	205	58	31	44	144	0.21	0.3945	0.256

$$+ C_{35}^2(C_{11}C_{22} - C_{12}^2) + C_{55}) > 0. \quad (1)$$

In this study, the crystal structure of P21/m-Ni₃Ta is monoclinic. According to the values from Table 2, the elastic constants of P21/m-Ni₃Ta do not satisfy with the mechanical stability criteria given by (1), which confirms that P21/m-Ni₃Ta is mechanical unstable.

The mechanical stability criteria for tetragonal structures can be expressed as follows [43]:

$$C_{11} > 0, C_{33} > 0, C_{44} > 0, C_{66} > 0, C_{11} - C_{12} > 0, \\ C_{11} + C_{33} - 2C_{13} > 0, 2C_{11} + C_{33} + 2C_{12} + 4C_{13} > 0. \quad (2)$$

In this work, five Ni–Ta intermetallic compound crystal structures (Ni₈Ta, I4/mmm-Ni₃Ta, Ni₂Ta, ha-NiTa₂ and hc-NiTa₂) are tetragonal crystals. For Ni₈Ta, I4/mmm-Ni₃Ta, Ni₂Ta and ha-NiTa₂, the elastic constants satisfy all stability criteria given by (2), which implies that these alloys are mechanically stable. However, for the hc-NiTa₂ structure, the elastic constants do not fulfill the restriction of $C_{11} > 0, C_{44} > 0, C_{11} - C_{12} > 0$ and $C_{11} + C_{33} - 2C_{13} > 0$. This indicates that the hc-NiTa₂ structure is a mechanically unstable structure, and it cannot exist at temperature of 0 K.

Next, the mechanical stability criteria for orthorhombic structures can be given by the following inequalities [44]:

$$C_{ij} > 0 (i=j, 0 < i \leq 6), C_{11} + C_{22} - 2C_{12} > 0, C_{11} + C_{33} - 2C_{13} > 0, \\ C_{22} + C_{33} - 2C_{23} > 0, C_{11} + C_{22} + C_{33} + 2C_{12} + 2C_{13} + 2C_{23} > 0. \quad (3)$$

As shown in Table 2, the elastic constants for orthorhombic Pmmn-Ni₃Ta satisfy all stability criteria given by (3), and this implies that Pmmn-Ni₃Ta is mechanically stable.

Finally, the mechanical stability conditions for hexagonal structures can be expressed as follows [45,46]:

$$C_{11} > 0, C_{44} > 0, C_{11} - C_{12} > 0, (C_{11} + C_{12})C_{33} - 2C_{13}^2 > 0. \quad (4)$$

For hexagonal NiTa considered in this paper, all values of elastic constants obey the mechanical stability conditions given by (4), which implies that the NiTa compound is mechanically stable.

Based on the above analysis, we conclude that, except for P21/m-Ni₃Ta and hc-NiTa₂, all other Ni-Ta intermetallic compounds considered here are mechanically stable.

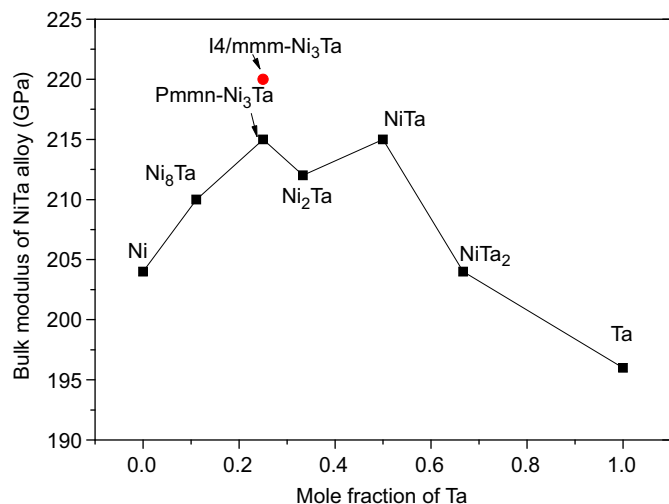


Fig. 3. Calculated bulk modulus of Ni-Ta intermetallic compounds.

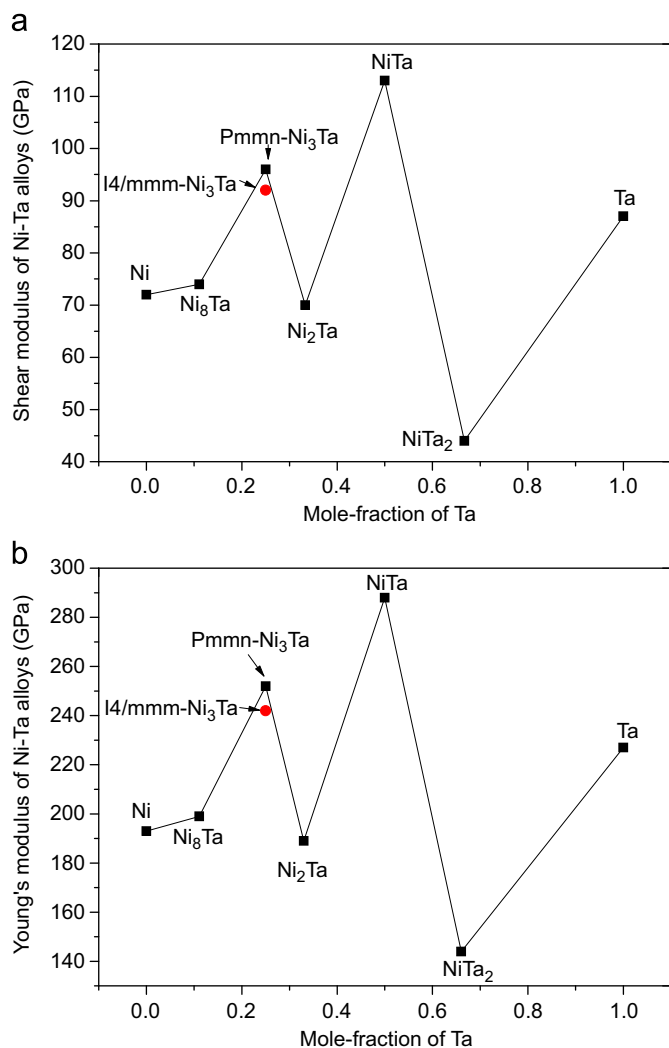


Fig. 4. Calculated shear modulus and Young's modulus of Ni-Ta intermetallic compounds.

To make further conclusions on the mechanical properties, polycrystalline bulk modulus (K), shear modulus (G), Young's modulus (E), and Poisson's ratio (ν) have been calculated by applying the Voigt-Reuss-Hill (VRH) approximation [47,48] for six mechanically stable Ni-Ta intermetallic compounds. For the convenience of the reader they are listed in Table 3. Fig. 3 shows the bulk modulus K with respect to the Ta concentration. As can be seen from Fig. 3, I4/mmm-Ni₃Ta has the highest bulk modulus, with the value of 220 GPa. Fig. 4 shows the Young's modulus E and shear modulus G against the Ta concentration. The variation trend for Young's modulus and shear modulus with Ta concentration are similar. In particular, NiTa has the highest E and G values of 288 GPa and 113 GPa, respectively, whereas the ha-NiTa₂ has the lowest E and G values of 144 GPa and 44 GPa, respectively.

In this work, brittleness and ductility properties of Ni-Ta intermetallic compounds have been studied by calculating the ratio of shear modulus to bulk modulus, G/K . This can be seen as an empirical criterion of the extent of fracture range in materials. A high value of G/K for a material may be associated with brittleness whereas a low value would correspond to ductility. The critical value that separates brittleness and ductility is around 0.57. That is to say, if G/K value is higher than 0.57 the material behaves in a brittle manner, otherwise the material behaves in a ductile manner [49]. Our calculated G/K values are 0.35, 0.42, 0.45, 0.33, 0.53, and 0.21 for Ni₈Ta, I4/mmm-Ni₃Ta, Pmmn-Ni₃Ta, Ni₂Ta, NiTa, and ha-NiTa₂, respectively. These results indicate that

Table 4

The heats of formation for Ni-Ta intermetallic compounds, calculated in this work known from the literature.

Compound	Heats of formation (KJ/mol atoms)	Reference
Ni ₈ Ta	-15.2026	This work
	-16.37	[8] CALPHAD
I4/mmm-Ni ₃ Ta	-28.3298	This work
	-35.29	[8] CALPHAD
	-29.7379	This work
Pmmn-Ni ₃ Ta	-34.81	[8] CALPHAD
	-17.8237	This work
Ni ₂ Ta	-22.36	[8] CALPHAD
	-25.6724	This work
NiTa	-25.51	[8] CALPHAD
	-17.5287	This work
ha-NiTa ₂	-21.75	[8] CALPHAD

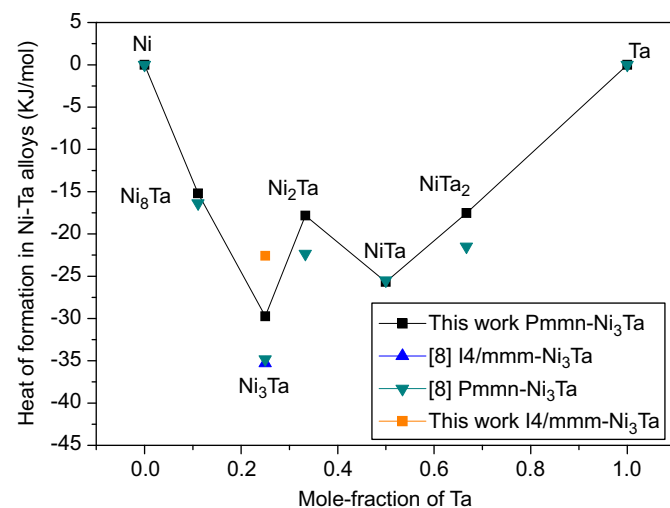


Fig. 5. The calculated heats of formation compared to former calculated values for Ni-Ta intermetallic compounds.

six mechanically stable Ni–Ta intermetallic compounds are ductile materials. Poisson's ratio is another characteristic to distinguish the ductility property of materials [50]. Materials with a Poisson's ratio around 1/3 are ductile, while materials with a Poisson's ratio far less than 1/3 are inferred as brittle. Based on our calculated Poisson's ratio, NiTa can be considered as a brittle material, while the other five mechanical stable Ni–Ta intermetallic compounds are ductile materials. We note also that Ni₃Ta has always brittle properties under experimental conditions, and the reason for its brittle properties may be attributed to the precipitates in grain boundaries [9]. Therefore, the single crystal production technology, powder metallurgy, strengthening the grain boundaries, and some other methods are worth a try to ameliorate the intergranular cracking. In this work, the hardness of intermetallics has also been determined based on the corresponding valence electron density. It is known that the high

valence electron density signifies high hardness [51]. Our calculated valence electron densities are 0.193, 0.224, 0.212, 0.227, 0.242, 0.256 electron/Å³ for Ni₈Ta, I4/mmm-Ni₃Ta, Pmmn-Ni₃Ta, Ni₂Ta, NiTa, NiTa₂, respectively. These results show that the hardness increases with the Ta concentration.

3.3. Thermodynamic stability and heats of formation

To study the thermodynamic properties, total energies of six mechanical stable Ni–Ta intermetallic compounds and the pure Ni, Ta have been obtained by DFT calculations. Then the heats of formation for Ni–Ta intermetallic compounds can be calculated on the basis of the following formula:

$$E_{\text{form}}^{\text{Ni}_m\text{Ta}_n} = (E_{\text{total}}^{\text{Ni}_m\text{Ta}_n} - mE_{\text{solid}}^{\text{Ni}} - nE_{\text{solid}}^{\text{Ta}}) / (m + n) \quad (5)$$

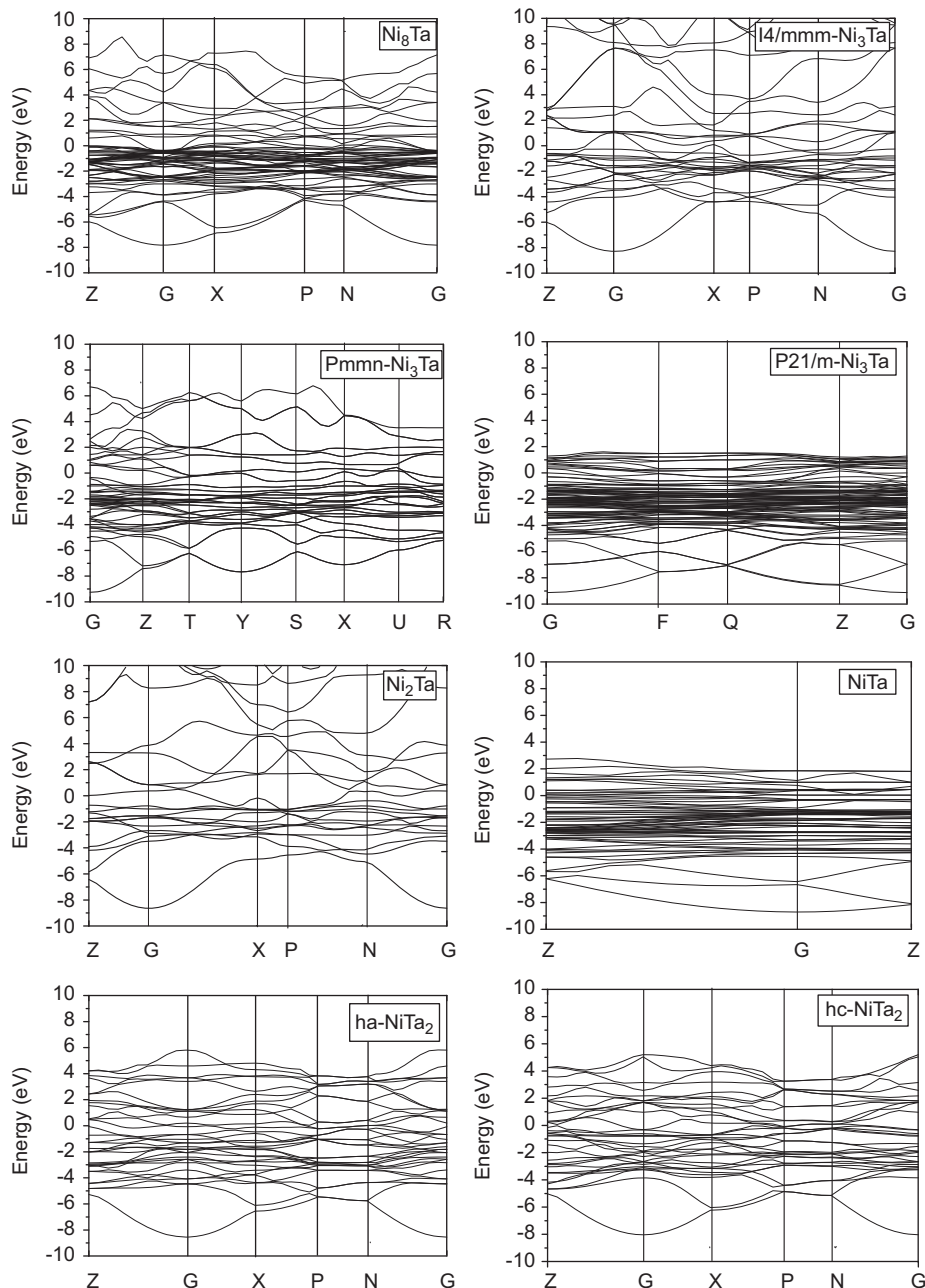


Fig. 6. Electronic energy bandstructures of Ni–Ta intermetallic compounds.

where $E_{\text{form}}^{\text{Ni}_m\text{Ta}_n}$ is the atomic heats of formation for a Ni_mTa_n alloy, $E_{\text{total}}^{\text{Ni}_m\text{Ta}_n}$ refers to the total energy of a Ni_mTa_n primitive cell that includes m Ni atoms and n Ta atoms with equilibrium lattice parameters, $E_{\text{solid}}^{\text{Ni}}$ is the total energy of a Ni atom with FCC structure, $E_{\text{solid}}^{\text{Ta}}$ is the total energy of a Ta atom with BCC structure.

Using the formula (5), the heats of formation for mechanically stable Ni-Ta intermetallic compounds have been calculated, and the results are summarized in Table 4 along with the previously known theoretical results found in the literature [8]. It can be seen that the calculated values are in a good agreement with such

results. This comparison is also visualized by Fig. 5. As seen in Fig. 5, all the heats of formation are negative, and the absolute values of heats of formation for Ni_8Ta , $I4/mmm\text{-Ni}_3\text{Ta}$, $\text{Pmmn-Ni}_3\text{Ta}$, $\text{P21/m-Ni}_3\text{Ta}$, Ni_2Ta , NiTa , and $\text{hc-Ni}_2\text{Ta}$ are 15.2, 22.6, 29.7, 17.8, 25.7, 17.5 kJ/mol atoms, respectively. These observations imply that the chemical interaction between Ni and Ta is not so tight, but the negative heats of formation ensure that these intermetallic compounds are thermodynamically stable. Nevertheless, Ni_2Ta can be considered as a thermodynamic unstable phases, due to the fact that it can be transformed into lower energy phases of Ni_3Ta and NiTa .

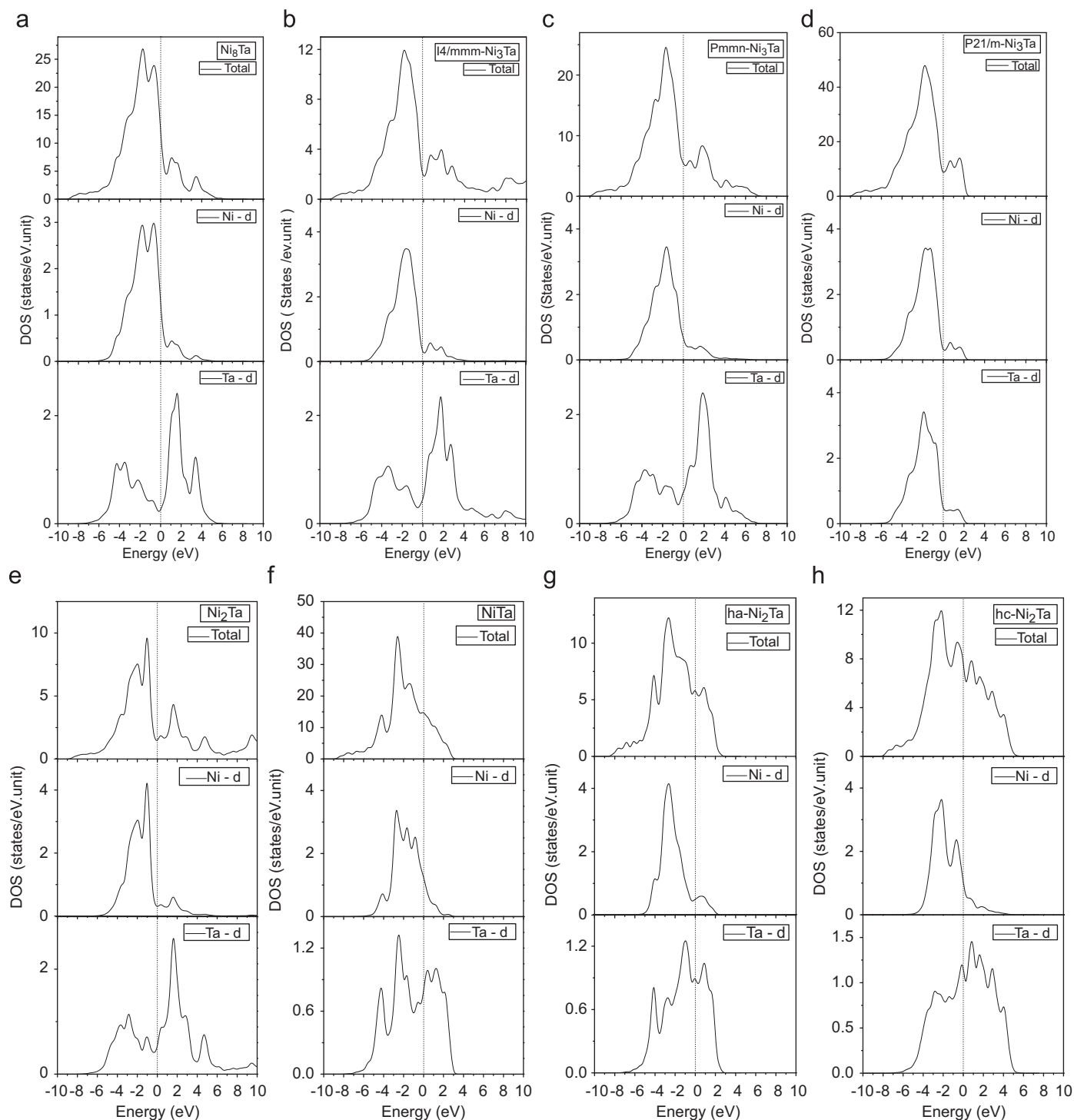


Fig. 7. Density of state for Ni-Ta intermetallic compounds.

3.4. Electronic energy band structure

In this work, the electronic energy band structures and density of states of the Ni–Ta intermetallic compounds have also been calculated, and they are shown in Figs. 6 and 7, respectively. Electronic energy band structures indicate the energy of point which has symmetry in our intermetallic system. The level at zero energy in Fig. 6 is the Fermi level, which is defined as the highest energy level is occupied by the electrons at 0 K, is located in the band gap. As seen in Fig. 6, the valence band overlaps the conduction band at the Fermi surface. Hence, the Ni–Ta intermetallic compounds considered here are all conducting materials. Besides, as it is indicated clearly in Fig. 7, peaks exist in the two sides of Fermi level. Furthermore, the density of states correspond to the Fermi level was not zero; imply that all the Ni–Ta intermetallics are conductors. According to the partial density of states, the main valence electron contributions of the bonding electrons in the whole regions are Ni(3d) and Ta(5d). Ta-d state and Ni-d state are hybridized in the valence band of these intermetallic compounds except Ni₂Ta, the valence band of which is occupied by Ni-d state. Moreover, the bond peaks above Fermi level are conduction band, which are mainly dominated by Ta-d valence electrons for I4/mmm–Ni₃Ta, Pmmn–Ni₃Ta, Ni₂Ta, ha–NiTa₂ and hc–NiTa₂, while that of NiTa and Ni₈Ta are occupied by Ni-d state. For I4/mmm–Ni₃Ta, the Ni-d state and Ta-d state have a hybridization in conduction band. In addition, the distance of the nearest peaks located separately in the two sides of zero energy symbolized the bands, with the increasing of distance, the bond transformed from metallic to covalent. These peaks are close to each other in Fig. 7, which demonstrate the metallicity of these intermetallic compounds. With the increasing of width, the pseudogap for these intermetallics can be sequenced in the order of ha–NiTa₂, Ni₂Ta, hc–NiTa₂, Ni₈Ta, P21/m–Ni₃Ta, I4/mmm–Ni₃Ta, Pmmn–Ni₃Ta and NiTa. The ductility of intermetallics may become weaker as the metallicity of bond reducing, consequently, NiTa has the weakest ductility among these alloys, while ha–NiTa₂ has the best ductility, the deformation ability of intermetallics enhanced with the increasing of pseudogap width. This trend is in accordance with the ductility testified by *G/K* and poisson's ratio values discussed above. As seen in Fig. 7, it is found that the bonding electron numbers per atom below the Fermi level are 9.53, 8.90, 8.87, 8.86, 8.45, 7.82, 6.80, 6.71 for Ni₈Ta, I4/mmm–Ni₃Ta, P21/m–Ni₃Ta, Pmmn–Ni₃Ta, Ni₂Ta, NiTa, ha–NiTa₂, hc–NiTa₂, respectively. The larger number of bonding electron, the stronger charge interaction [52,53], and the structural stability of alloy will be better. Thus, the structure stability increases with the Ta concentration.

4. Conclusions

In conclusion, we have investigated the structural properties, elastic properties, heats of formation and electronic structures for five Ni–Ta binary intermetallic compounds by utilizing DFT calculations. Our optimized lattice parameters agree well with available experimental values. The mass density of Ni–Ta intermetallic compounds increases approximately in a linear manner with the increasing Ta concentration. All the Ni–Ta intermetallic compounds considered here are mechanically stable, except for P21/m–Ni₃Ta and hc–NiTa₂. The polycrystalline elastic modulus and Poisson's ratio have been deduced by the VRH approximation, and the calculated *G/K* values indicated that Ni₈Ta, I4/mmm–Ni₃Ta, Pmmn–Ni₃Ta, Ni₂Ta, NiTa, ha–NiTa₂ are ductile materials. The calculated heats of formation for Ni–Ta intermetallic compounds demonstrate that Ni₂Ta is a thermodynamic unstable phase. Our results have also indicated that Pmmn–Ni₃Ta is the

ground stable phase of Ni₃Ta polymorphs. The energy band structures calculated in this work demonstrate that all five Ni–Ta intermetallic compounds are conductors. The ductility of Ni–Ta intermetallic compounds deduced from the density of state corresponds very well with the result derived from the *G/K* and poisson's ratio. The structure stability increases with the Ta concentration.

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